

CLAIM AMENDMENTS

1 1. (Currently amended) A method for rapid tomographic
2 measurement of conductivity distribution in a sample, comprising
3 the steps of:

4 (a) launching electrical excitation signals
5 simultaneously into a sample from a multiplicity of locations
6 distributed in said sample;

7 (b) measuring at a multiplicity of locations in said
8 sample at least one parameter selected from the group which
9 consists of potential difference and magnetic field strength
10 resulting from said electrical excitation signals; and

11 (c) correlating the measured potential differences or
12 magnetic field strengths with the launched excitation signals to
13 provide conductivity distribution cross section in said sample.

14 wherein the electrical excitation signals are launched as
15 orthogonal signals into said sample; and

16 (d) wherein the electrical excitation signals are
17 launched as orthogonal signals into said sample.

Claim 2 (cancelled).

1 3. (Currently amended) The method defined in claim
2 [[2]] 1 wherein the electrical excitation signals are launched as
3 orthogonal sinusoidal signals into said sample.

1 4. (original) The method defined in claim 3 wherein in
2 the measurement of said parameter at least one voltage component
3 a_i , b_i is determined using a defining equation of the Fourier-
4 analysis cosine coefficients according to the formula:

$$a_i = \frac{2}{T} \int_0^T U_G(t) \cos(i\omega_0 t) dt$$

5 where a_i = peak value of the measured voltage amplitude;

6 ω_0 = fundamental frequency of the excitation signal;

7 i = the index of the excitation signal from 1 to ∞ ;

8 $U_G(t)$ = measured potential difference; and

9 t = time

10 or

11 using a defining equation
12 of the Fourier-analysis sine coefficients according to the
13 formula:

$$b_i = \frac{2}{T} \int_0^T U_G(t) \sin(i\omega_0 t) dt$$

14 where b_i = peak value of the measured voltage amplitude phase
15 shifted by 90° ;
16 ω_0 = fundamental frequency of the excitation signal;
17 i = the index of the excitation signal from 1 to ∞ ;
18 $U_0(t)$ = measured potential difference; and
19 t = time.

1 5. (Original) The method defined in claim 4 wherein the
2 coefficients a_i , b_i are used to calculate a complex impedance of the
3 sample.

1 6. (Original) The method defined in claim 1 wherein the
2 excitation signals launched into said sample are coded signals.

1 7. (Original) The method defined in claim 1 wherein the
2 excitation signals launched into said sample can assume either of
3 only two possible amplitudes.

1 8. (Original) The method defined in claim 1 wherein at
2 least three electrodes in spaced apart relationship are inserted
3 into said sample for launching said excitation signals into said
4 sample.

5 9. (Original) The method defined in claim 1 wherein at
6 least two electrodes in spaced apart relationship are inserted into
7 said sample for measuring potential differences therein.

1 10. (Original) The method defined in claim 1 wherein at
2 least three electrodes in spaced apart relationship are inserted
3 into said sample for launching said excitation signals into said
4 sample and at least two electrodes in spaced apart relationship are
5 inserted into said sample for measuring potential differences
6 therein, said electrical excitation signals are applied to said
7 sample at least a part of the three electrodes so that a potential
8 distribution occurs in the sample and potential differences are
9 measured at said at least two electrodes.

1 11. (Original) The method defined in claim 10 wherein
2 said electrical excitation signals are applied simultaneously to
3 said at least three electrodes and the measured potential
4 differences are correlated proportionally with supplied electrical
5 excitation signals.

1 12. (Original) The method defined in claim 1 wherein the
2 electrical excitation signals are launched into said sample from

3 the same electrodes with which measurements of the potential
4 differences are made.

1 13. (Original) The method defined in claim 1 wherein
2 said electrodes are spikes driven into the sample and having
3 electrically decoupled surfaces for applying said electrical
4 excitation signals to said sample and measuring potential
5 differences therein.

1 14. (Original) The method defined in claim 1 wherein
2 said electrical excitation signals are applied with a high-ohmic
3 current source.

1 15. (Original) The method defined in claim 1, further
2 comprising exciting said sample by energizing two coils in contact
3 with said sample.

1 16. (Original) The method defined in claim 1 wherein a
2 magnetic field strength is measured by a magnetic field sensor
3 brought into contact with said sample.

1 17. (Original) The method defined in claim 1 wherein the
2 electrical excitation signals are applied to at least part of a
3 plurality of excitation coils or excitation electrodes in contact
4 with the sample and as a result of conductivity distribution
5 therein a current density distribution and consequent magnetic
6 field strength distribution are effected in the sample.

1 18. (Original) The method defined in claim 1 wherein the
2 electrical excitation signals are applied to at least part of a
3 plurality of excitation coils or excitation electrodes in contact
4 with the sample and a correlation is made between a measured field
5 strength distribution in proportion to the electrical excitation
6 signals supplied.

1 19. (Original) The method defined in claim 1 wherein at
2 least two of said electrodes for measuring potential difference and
3 at least one magnetic field sensor for measuring a magnetic field
4 strength are provided in said sample.

1 20. (Original) The method defined in claim 1 wherein at
2 least three electrodes for applying an electrical excitation to
3 said sample and at least one magnetic field sensor for measuring a

4 magnetic field strength are provided in contact with said sample.

1 21. (Original) The method defined in claim 1 wherein
2 said electrical excitation signals are formed by an alternating
3 current fed to said sample.

1 22. (Original) The method defined in claim 1 wherein
2 electrical excitation signals in the form of an alternating voltage
3 are fed to the sample and the current amplitude in a conductor
4 feeding said electrical excitation signals to the sample is
5 measured.

1 23. (Currently amended) An apparatus for the rapid
2 tomographic measurement of a conductivity distribution in a sample,
3 comprising:

4 an electrical excitation source coupled with said sample
5 for applying electrical excitation signals thereto;

6 at least one device coupled with said sample for
7 measuring a potential difference or magnetic field strength therein
8 in proportion to the electrical excitation signals supplied
9 thereto; and

10 circuitry for correlating a measured potential difference

11 or magnetic field strength proportionally with the supplied
12 electrical excitation signals; and
13 wherein said circuitry includes a control and computing
14 unit which produces electrical orthogonal excitation signals and
15 enabled a correlation of measured potential differences or magnetic
16 field strengths proportionally with the electrical orthogonal
17 excitation signals.

Claim 24 (cancelled).

1 25. (Currently amended) The apparatus defined in claim
2 [[24]] 23 wherein said control and computing unit comprises at
3 least two generators for producing orthogonal electrical excitation
4 signals.

1 26. (Original) The apparatus defined in claim 25,
2 further comprising conductors for supplying said electrical
3 excitation signals to the sample.

1 27. (Original) The apparatus defined in claim 26 wherein
2 said circuitry includes an evaluation unit for calculating a
3 conductivity distribution in said sample.

4 28. (Original) The apparatus defined in claim 27 wherein
5 the electrical excitation source comprises at least three
6 electrodes engaged in said sample and in spaced-apart relationship.

1 29. (Original) The apparatus defined in claim 28 wherein
2 said at least one device comprises at least two electrodes in said
3 sample for measuring electromagnetic fields therein.

1 30. (Original) The apparatus defined in claim 23 wherein
2 the electrical excitation source comprises at least three
3 electrodes engaged in said sample and in spaced-apart relationship,
4 said electrodes being so configured as to enable a potential
5 difference measurement between said electrodes.

6 31. (Currently amended) An apparatus for the rapid
7 tomographic measurement of a conductivity distribution in a sample,
8 comprises:

9 an electrical excitation source coupled with said sample
10 for applying electrical excitation signals thereto;

11 at least one device coupled with said sample for
12 measuring a potential difference or magnetic field strength therein
13 in proportion to the electrical excitation signals supplied

14 thereto; and

15 circuitry for correlating a measured potential difference
16 or magnetic field strength proportionally with the supplied
17 electrical excitation signals, said electrodes being in the form of
18 spikes having excitation electrode surfaces electrically decoupled
19 from potential measuring surfaces respectively along jackets and
20 tips of the respective electrodes, The apparatus defined in claim
21 30 wherein said electrodes [[are]] being in the form of spikes
22 having excitation electrode surfaces electrically decoupled from
23 potential measuring surfaces respectively along jackets and tips of
24 the respective electrodes.

1 32. (Original) The apparatus defined in claim 23 wherein
2 said source includes at least two coils as the exclusive source of
3 excitation signals or in conjunction with excitation electrodes.

1 33. (Original) The apparatus defined in claim 23 wherein
2 said device includes at least one magnetic field sensor as the
3 exclusive means for measuring magnetic field strength or in
4 conjunction with at least one electrode.

1 34. (Original) The apparatus defined in claim 23 wherein
2 said circuitry includes a separating stage which decomposes the
3 measured signals in proportion to the applied electrical excitation
4 signals.